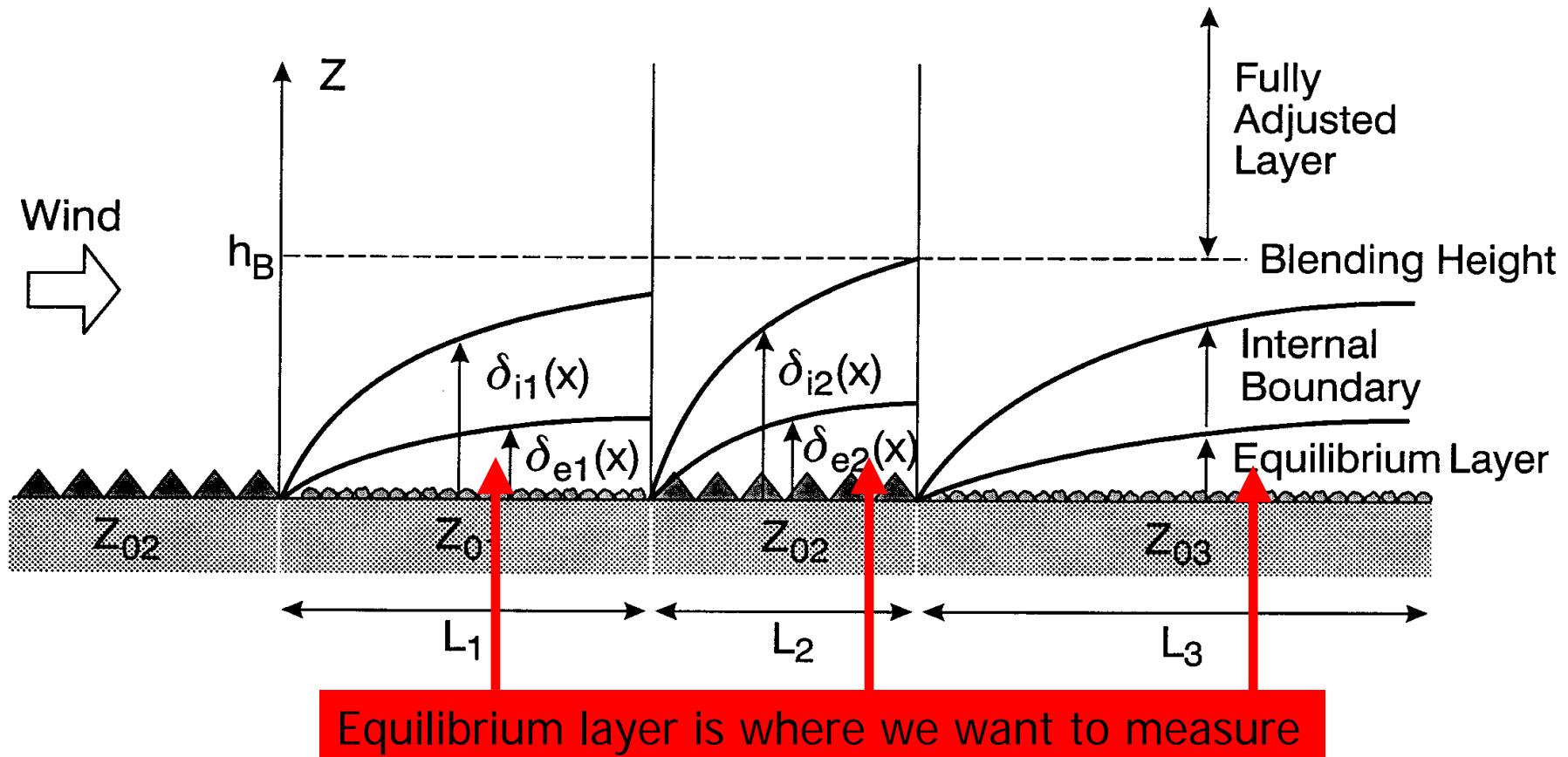


## Lecture 4: Site & Measurement requirements

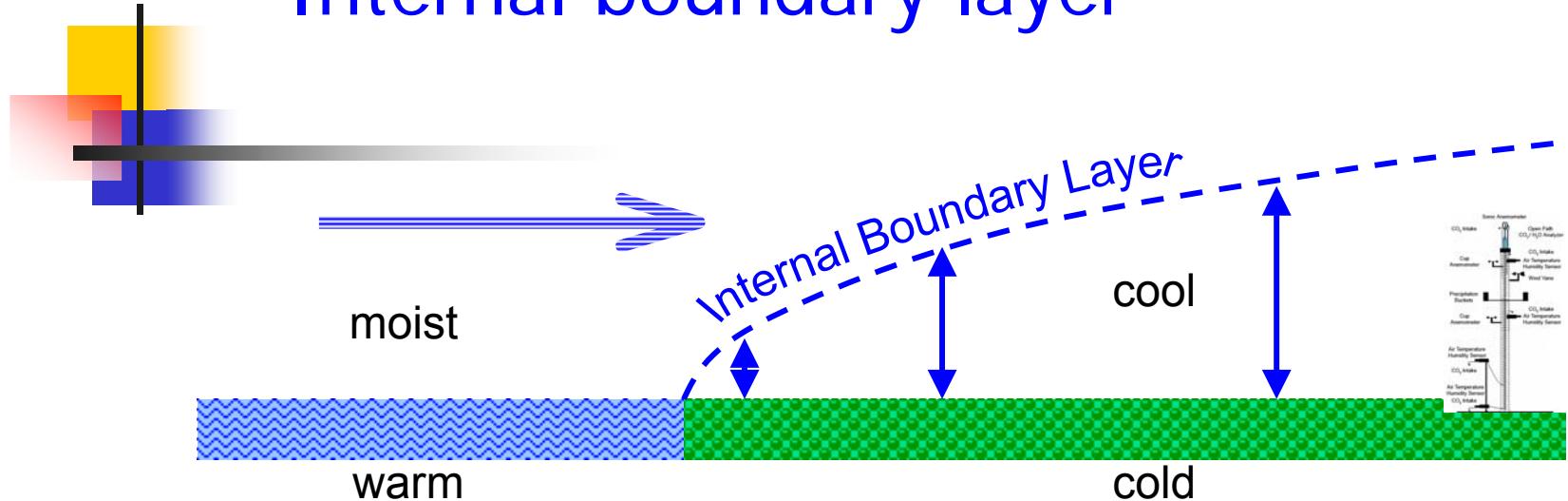
- Site requirements
  - Internal boundary layer
  - Flux footprint
- Measurement requirements
  - Eddy fluxes
  - Profiles
    - Vertical advection
    - Change in storage
- Energy closure

# Landscape is a patchwork of surfaces



Courtesy Dr JJ Finnigan, CSIRO

# Internal boundary layer



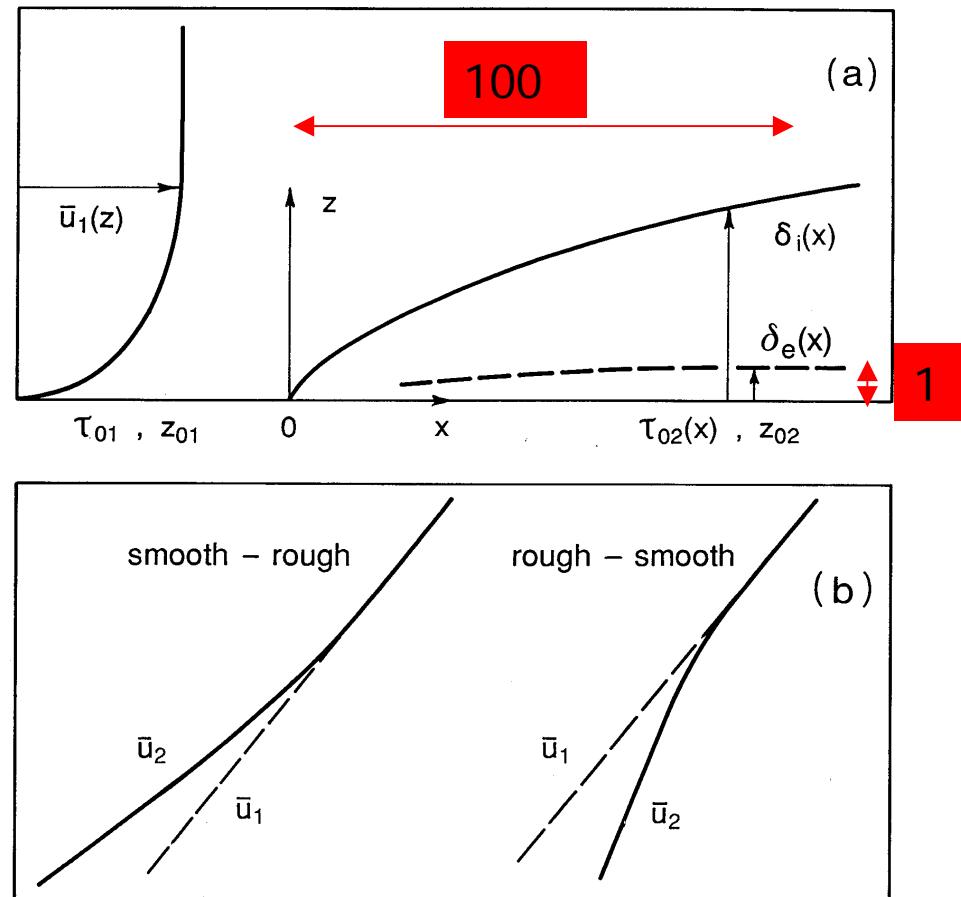
*“The depth over which the surface BL adjusts to new surface conditions is related to time it is allowed to do so”*

*“The strength of a thermal adjustment depends on the magnitude of the thermal forcing”*

Courtesy Prof HP Schmid  
Indiana University

# Windspeed adjustment to change in roughness

- 100:1 fetch rule of thumb
  - Neutral conditions
  - > for stable conditions
  - < for unstable conditions
- there is often a trade-off between a representative footprint and avoiding advective effects

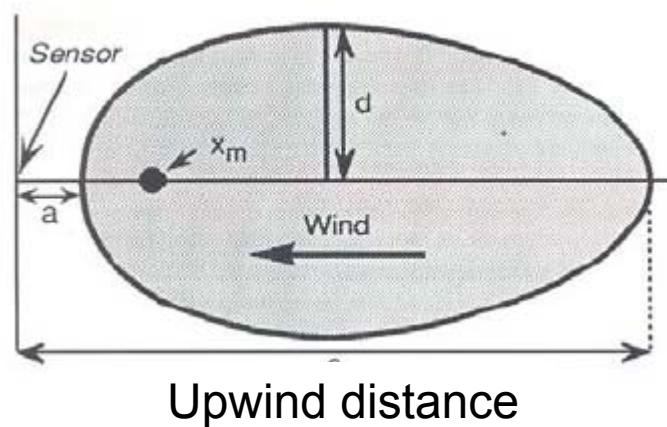
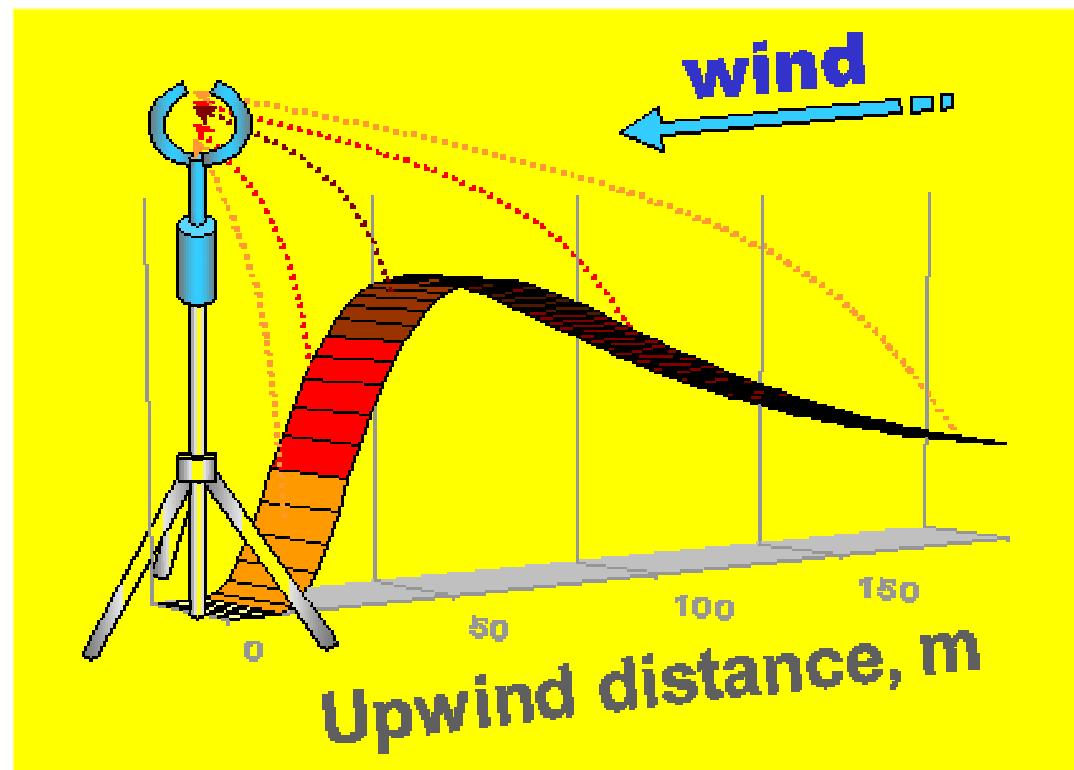


Courtesy Dr JJ Finnigan, CSIRO

Courtesy Prof HP Schmid Indiana University

## Source Footprint

*The area under the curve is contribution of source to the flux*



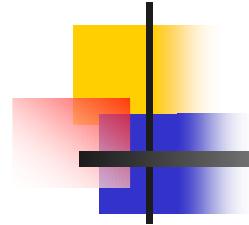
*Dimensions of the footprint area.*

$x_m$ : location of maximum source contribution

$a$ : downwind edge

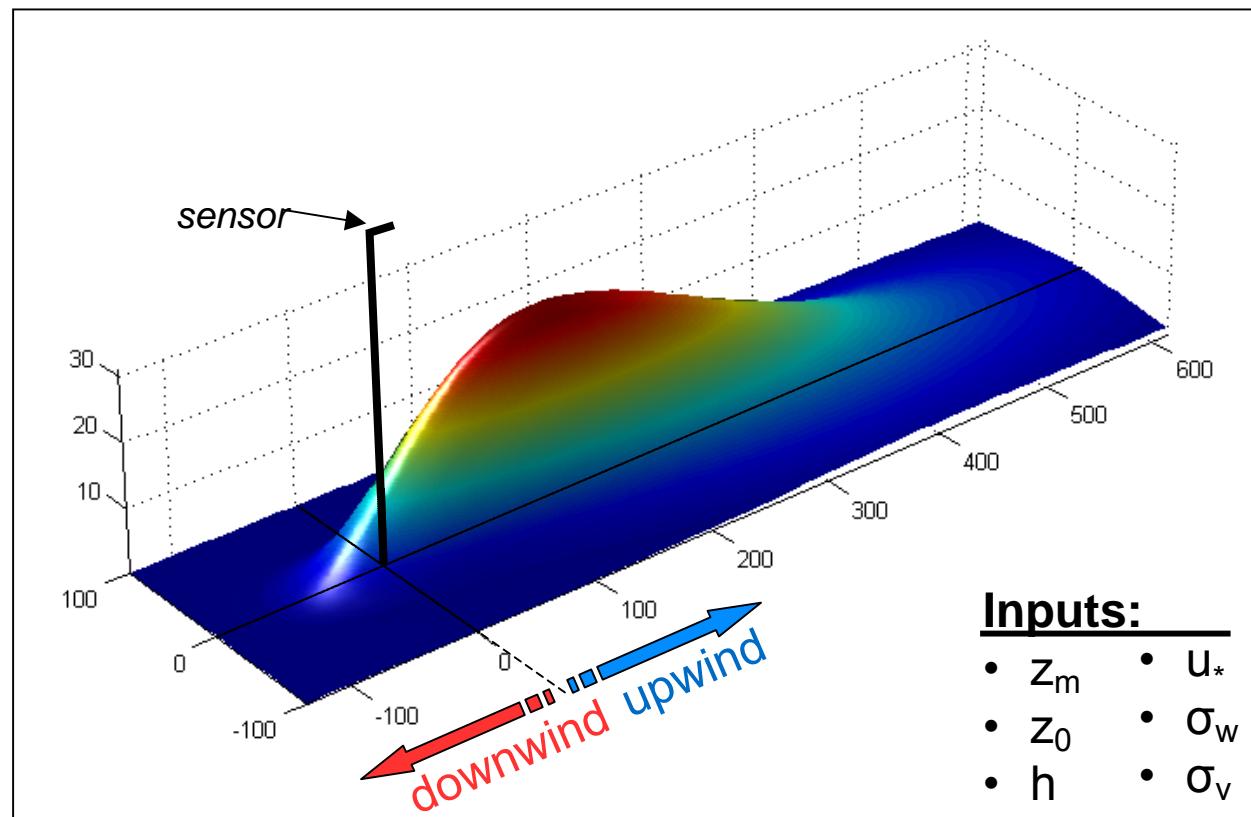
$d$ : lateral half-width area

Flux Footprint = spatial **filter**, "field of view"



$$F(\mathbf{x}) = \iint_{\mathbb{R}^2} Q_s(\mathbf{x}') \cdot f(\mathbf{x} - \mathbf{x}') \cdot d\mathbf{x}' = Q_s * f$$

(Convolution of the **source distribution**,  
 $Q_s$ , with the **footprint**,  $f$ )



Schmid 1994 (*Boundary-Layer Meteorol.*, **67**, 293-318)

Courtesy Prof  
HP Schmid  
Indiana  
University

# Cumulative flux footprint

Courtesy Prof HP Schmid Indiana University

$$\frac{F}{S_0} = \exp\left(\frac{-1}{k^2 x} D z^P |L|^{1-P}\right)$$

$F$  = measured flux

$S_0$  = surface source strength

$x$  = upwind distance,  $z$  = measurement height

$k$  = von Karman constant = 0.4

$L$  = Monin-Obukhov length

$D = 0.28; P = 0.59$

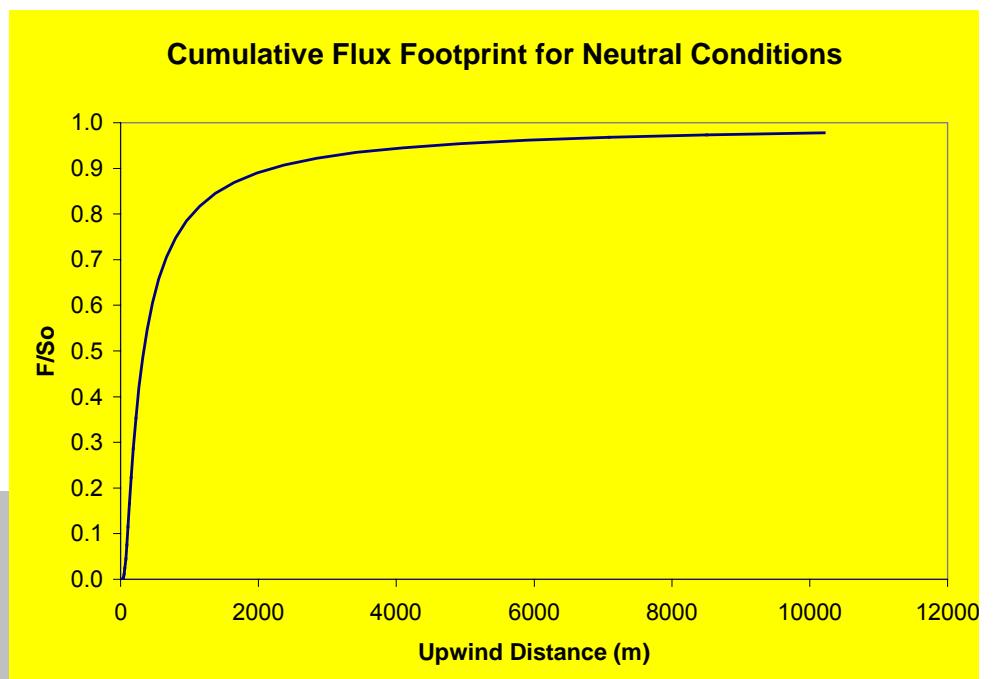
for unstable conditions ( $\xi = z_m / L < 0$ )

$D = 0.97; P = 1$

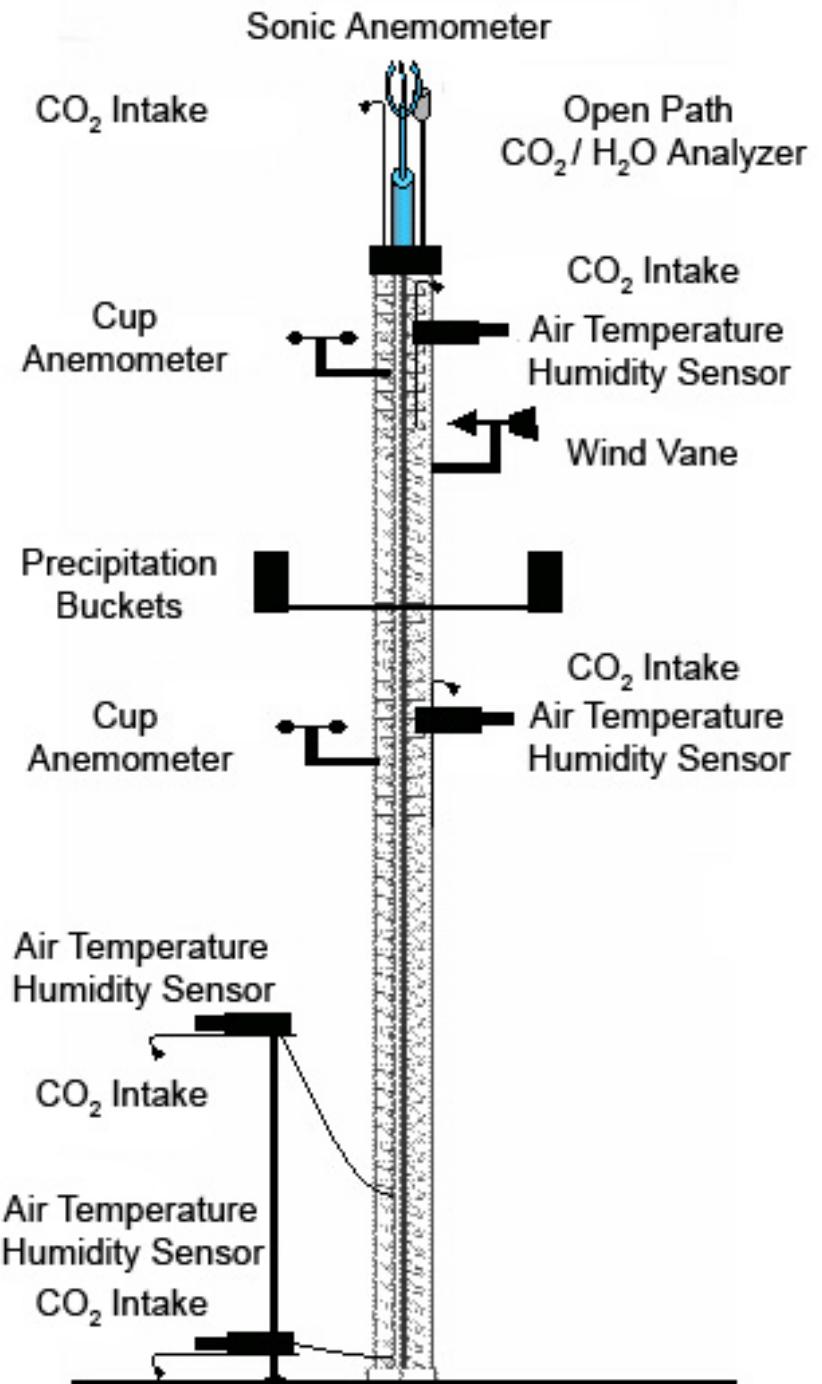
for near neutral conditions ( $|\xi| < 0.02$ )

$D = 2.44; P = 1.33$

for stable conditions ( $\xi > 0$ )



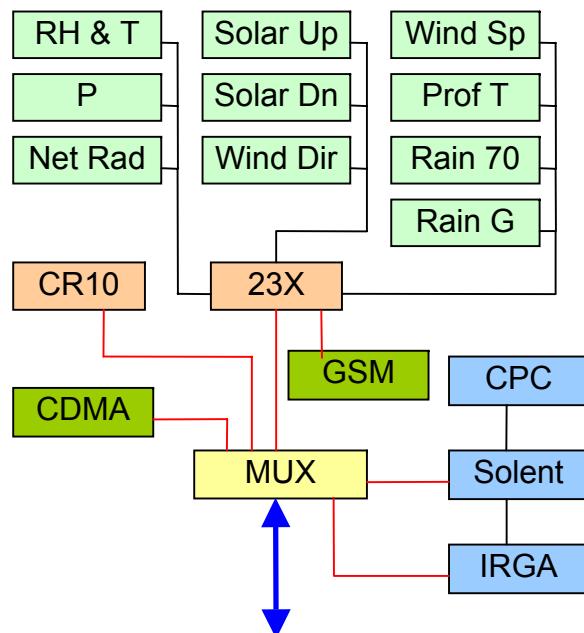
# Tower schematic



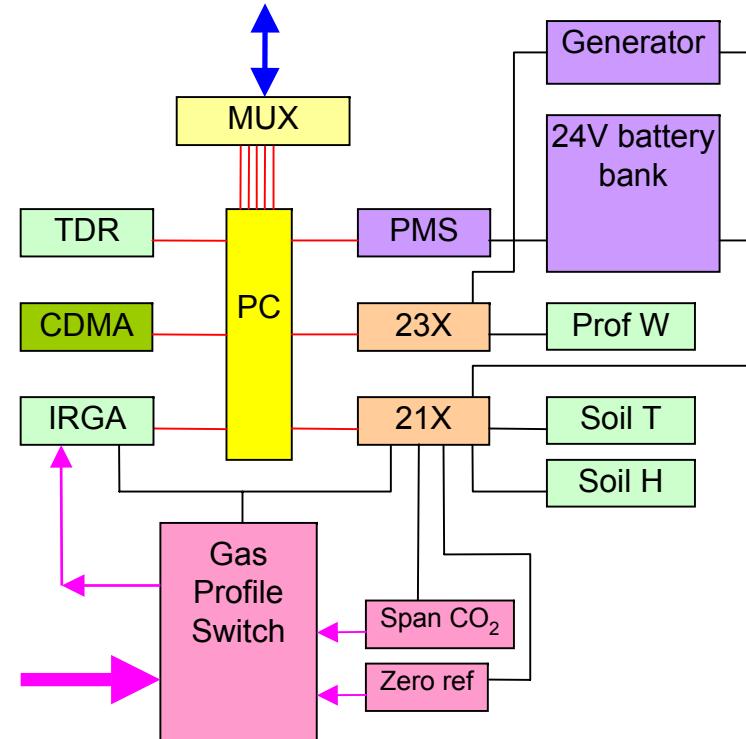
Courtesy Prof Shashi  
Verma, Univ. Nebraska

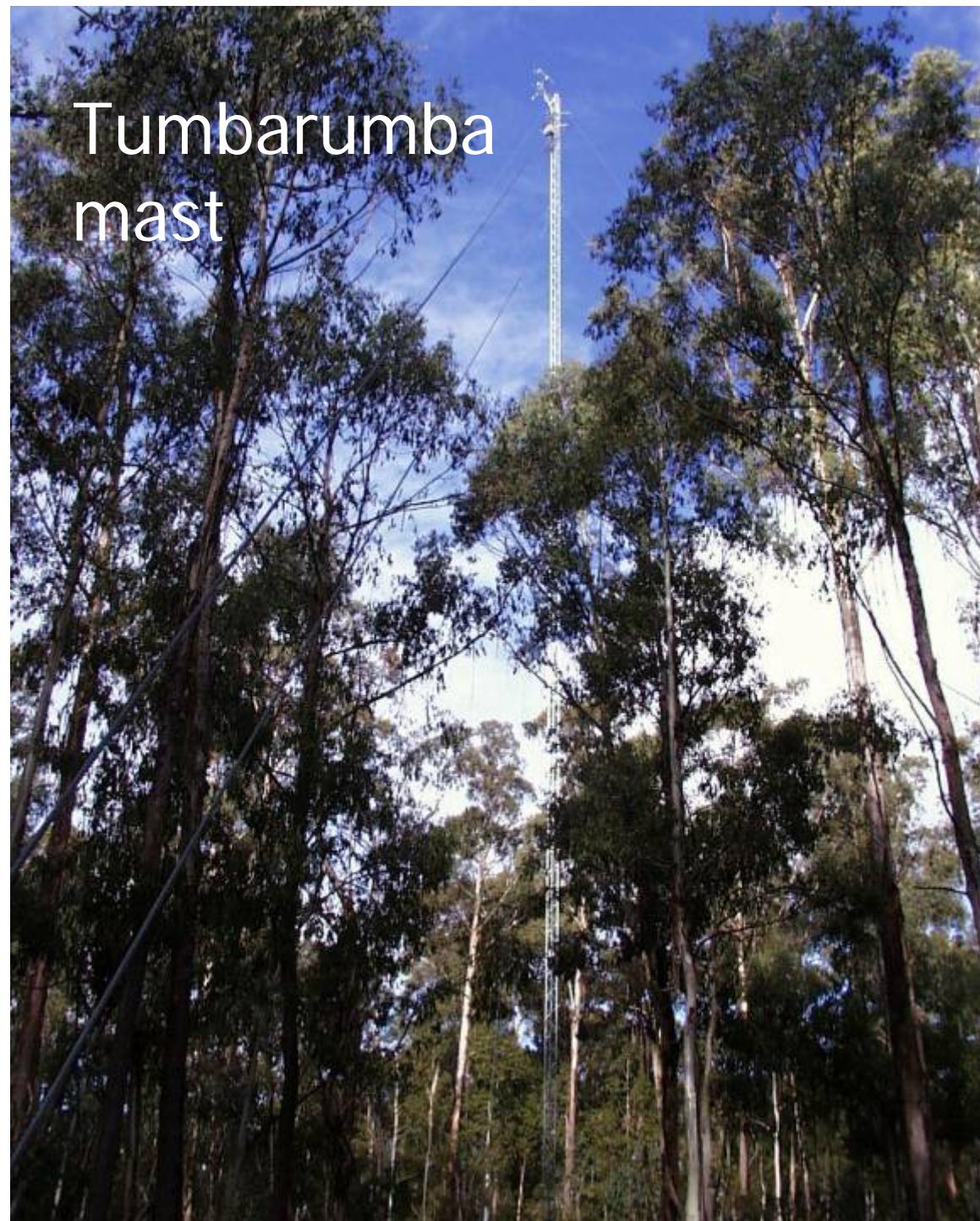
# Tumbarumba data acquisition

## Mast Instruments



## Ground Instruments

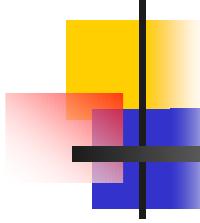


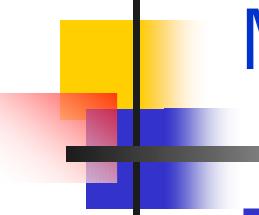


Tumbarumba  
mast



# Tumbarumba mast instruments





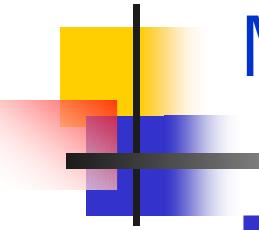
# Minimum measurements needed

## ■ Top of mast

- 3-D wind vector (20Hz)
- CO<sub>2</sub> and H<sub>2</sub>O concentrations (20Hz)
- Net radiation (15 min average)
- Incoming and reflected solar radiation (15 minute average)
- RH and air temperature (15 minute average)
- Wind speed and direction (15 minute average)
- Rainfall

## ■ Ground

- Soil temperature (15 minute average)
- Soil heat flux (15 minute average)
- Soil moisture (TDR, hourly)



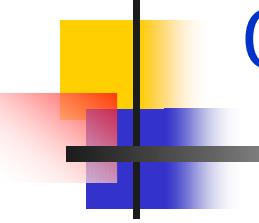
## Minimum measurements needed (cont<sup>d</sup>)

- Profiles (multiple levels, 1 Hz)

- Temperature
  - CO<sub>2</sub>
  - H<sub>2</sub>O vapor
  - 2- or 3-D wind vectors

# Instruments



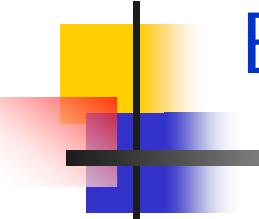


## Optional measurements

- Spectrometer (plant canopy reflectance spectra)
- Particle counter (VOC's, dust)
- Gas isotope measurements
- Etc., etc., etc.

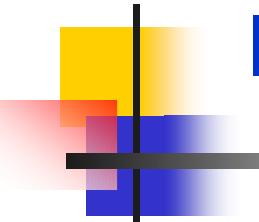
### **Limitations on instrumentation:**

- Power requirements
- Ability to maintain and calibrate the instruments !!



# Biological measurements

- Respiration chambers
  - Soil
  - leaves
  - Stems
- Photosynthesis chambers
- Carbon stocks
  - Soil
  - Biomass
- Allometric relationships
  - e.g. leaf biomass vs dbh
  - e.g. stem biomass vs dbh

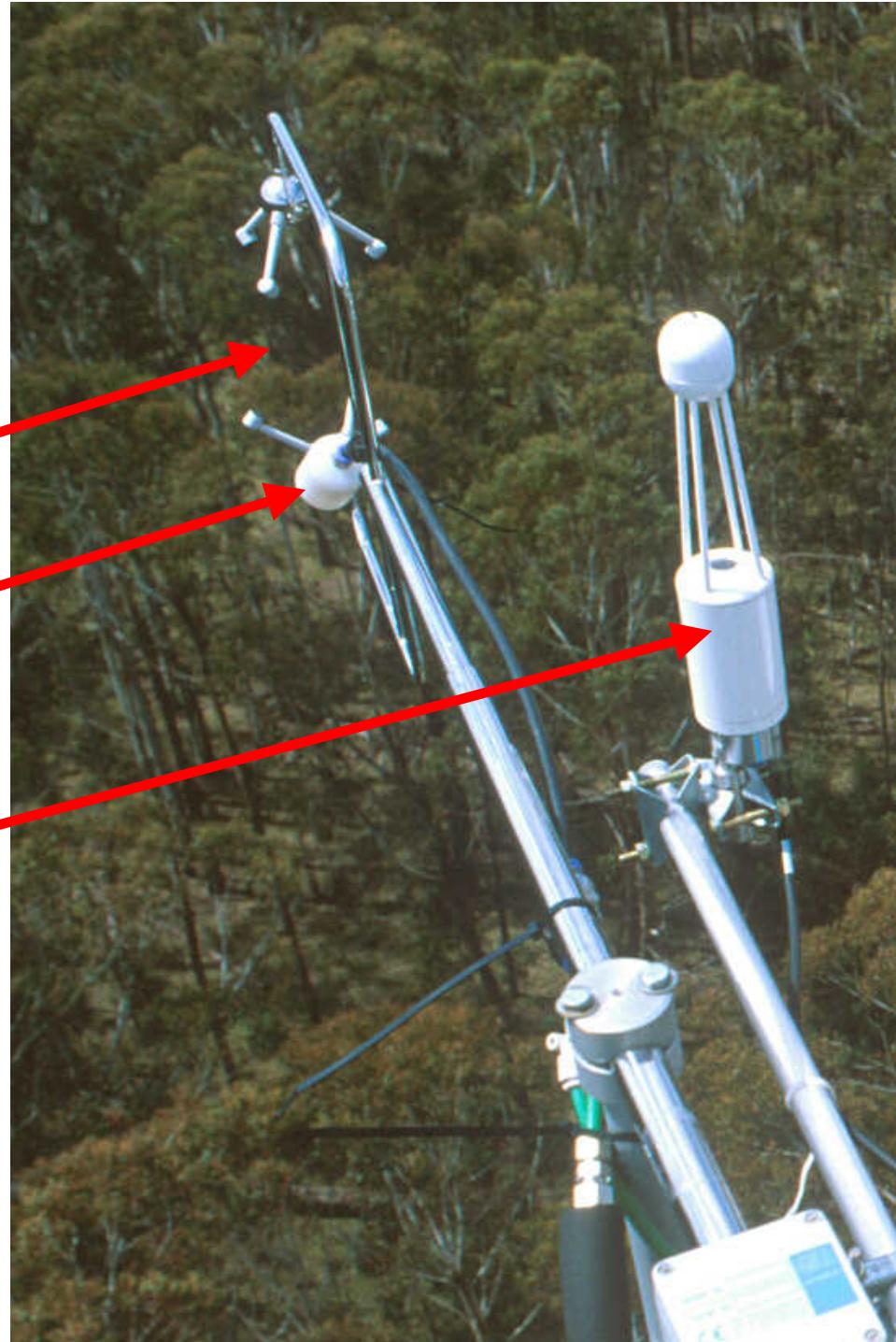


## Instrumentation

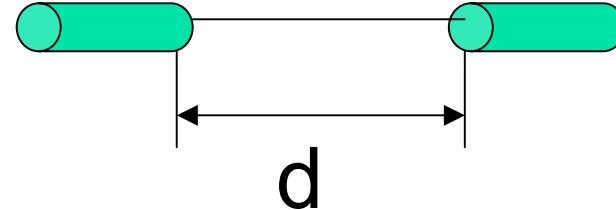
Sonic anemometer

Air intake for  
closed-path  $\text{CO}_2$  &  
 $\text{H}_2\text{O}$  analyser

Open-path  $\text{CO}_2$   
&  $\text{H}_2\text{O}$  analyser



# Sonic anemometer



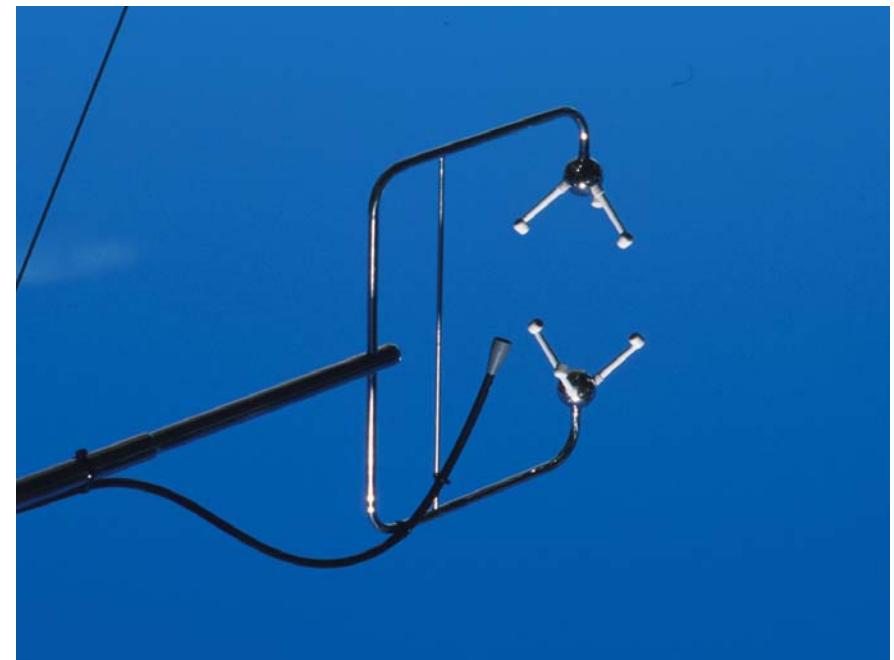
Wind speed

$$v_d = \frac{d}{2} \left[ \frac{1}{t_1} - \frac{1}{t_2} \right]$$

Absolute instrument for  $v_d$

Virtual temperature

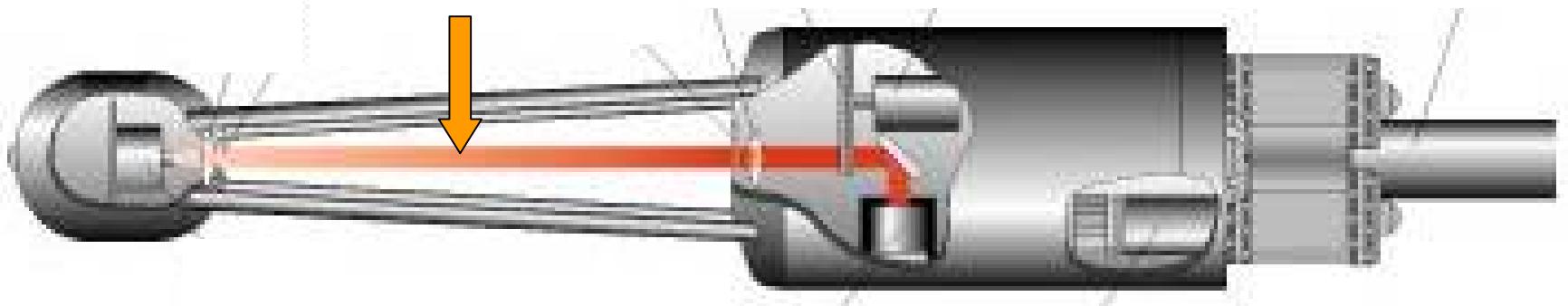
$$T_v = \frac{d^2}{1612} \left[ \frac{1}{t_1} + \frac{1}{t_2} \right]^2 + \frac{1}{403} \left[ v_x^2 + v_y^2 \right]$$



Kaimal & Finnigan, 1994

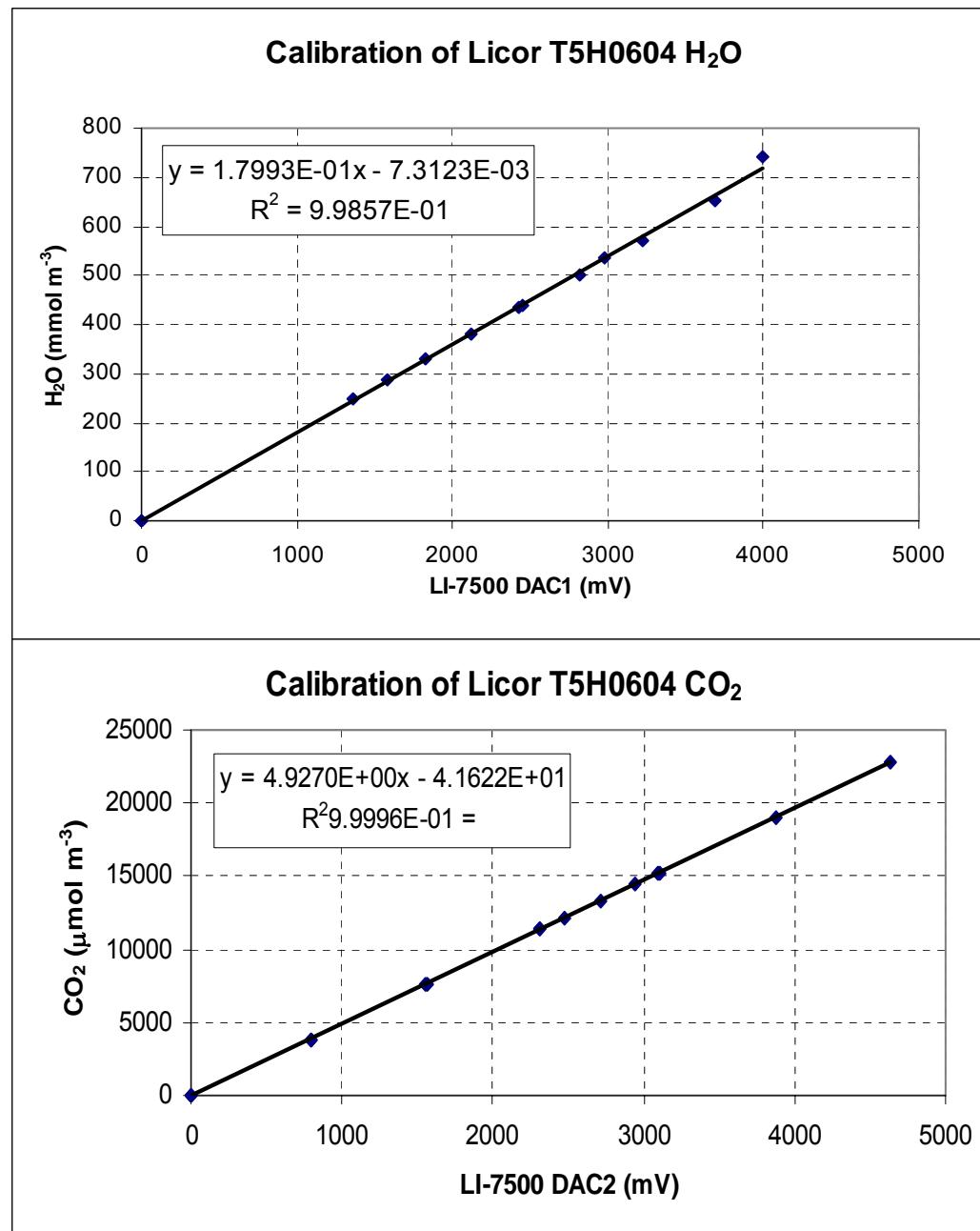
# Fast-response CO<sub>2</sub> and water vapor analyser

- Measures mol m<sup>-3</sup>  
in optical path

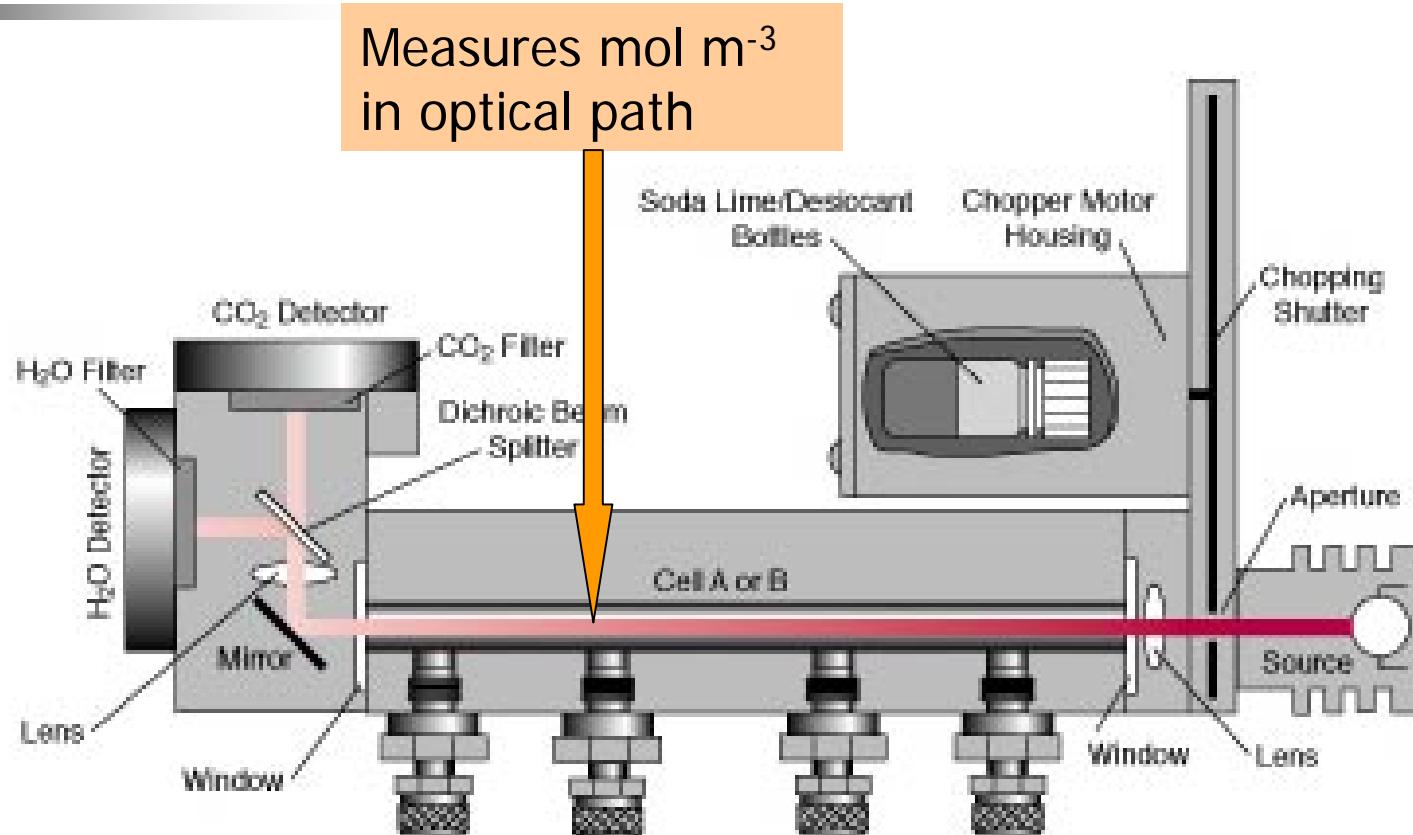


LI-7500 Open-path CO<sub>2</sub> and water vapor analyser

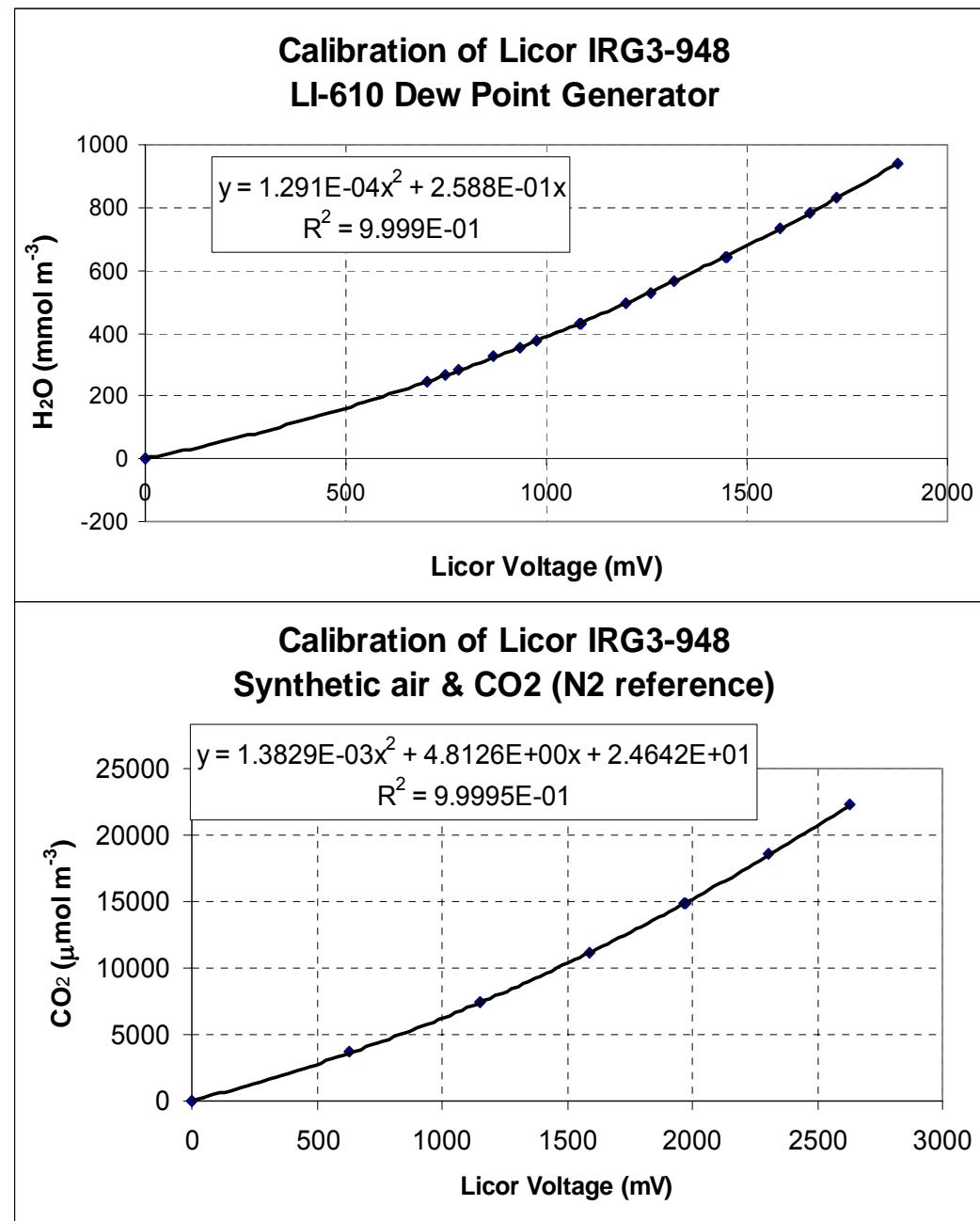
# Calibration LI-7500



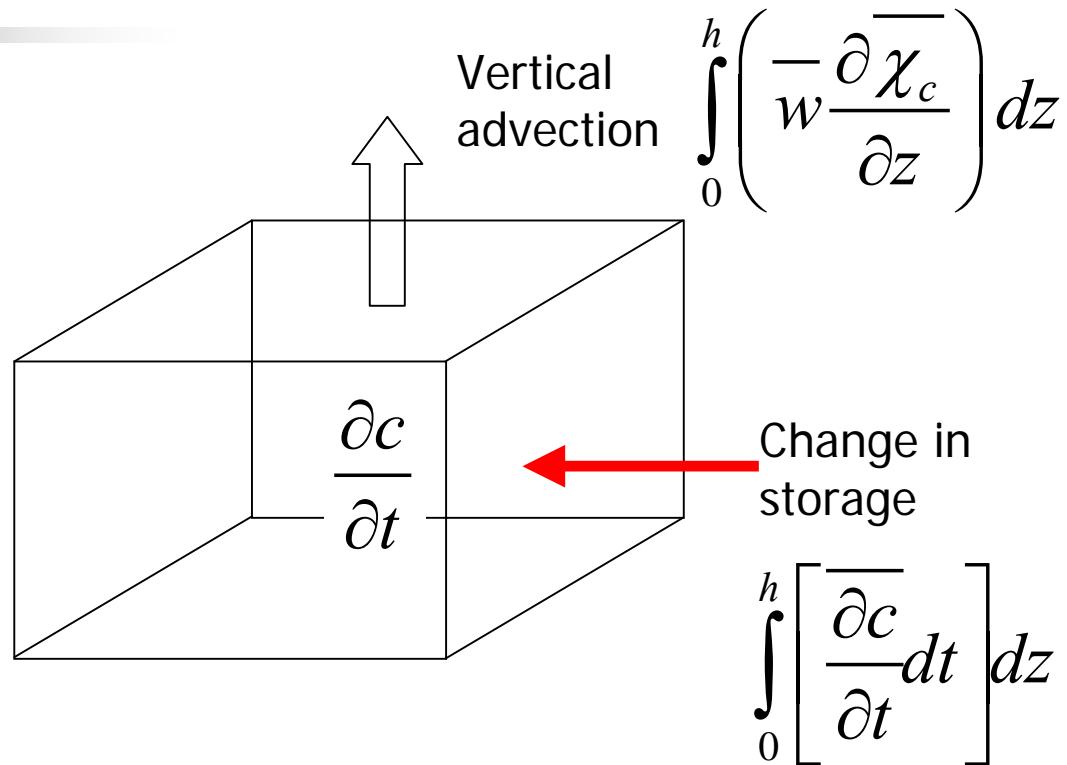
# Licor closed-path analyser



# Calibration LI-6262

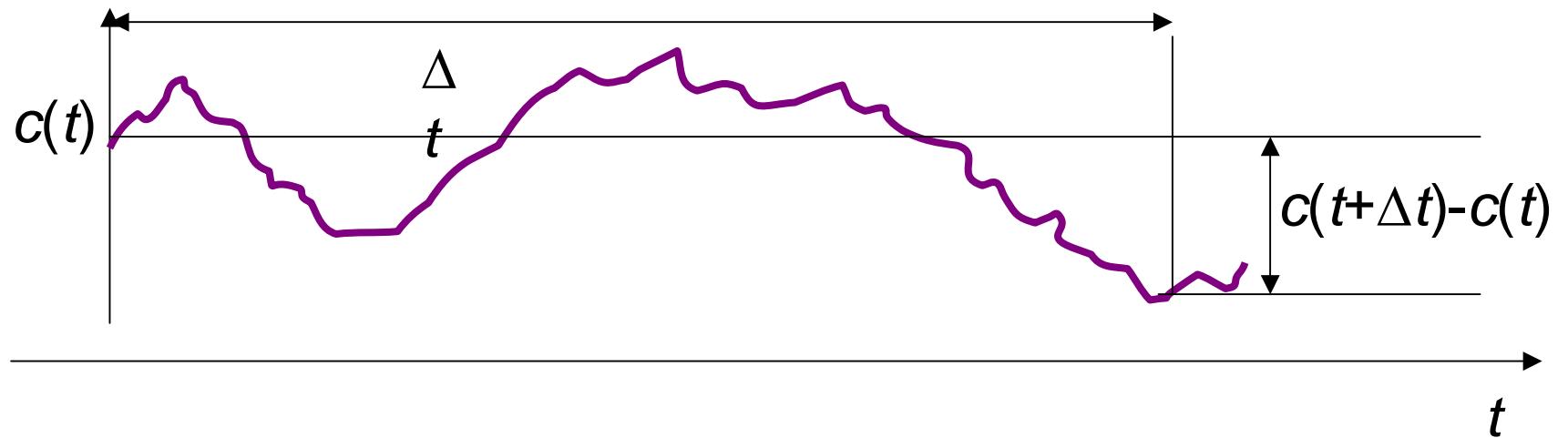


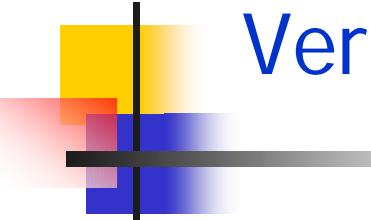
# Control volume



## The change in storage term

$$\int_0^h \left[ \frac{\partial c}{\partial t} dt \right] dz = \int_0^h \left[ \frac{1}{T} \int_0^T \frac{\partial c}{\partial t} dt \right] dz = \int_0^h \left[ \frac{1}{T} (c(T) - c(0)) \right] dz$$





# Vertical advection

See lecture 7 for details

$$\int_0^h \left( -\bar{w} \frac{\partial \bar{\chi}_c}{\partial z} \right) dz = \bar{w}(h) \bar{\chi}_c(h) - \int_0^h \left( \bar{\chi}_c \frac{\partial \bar{w}}{\partial z} \right) dz$$

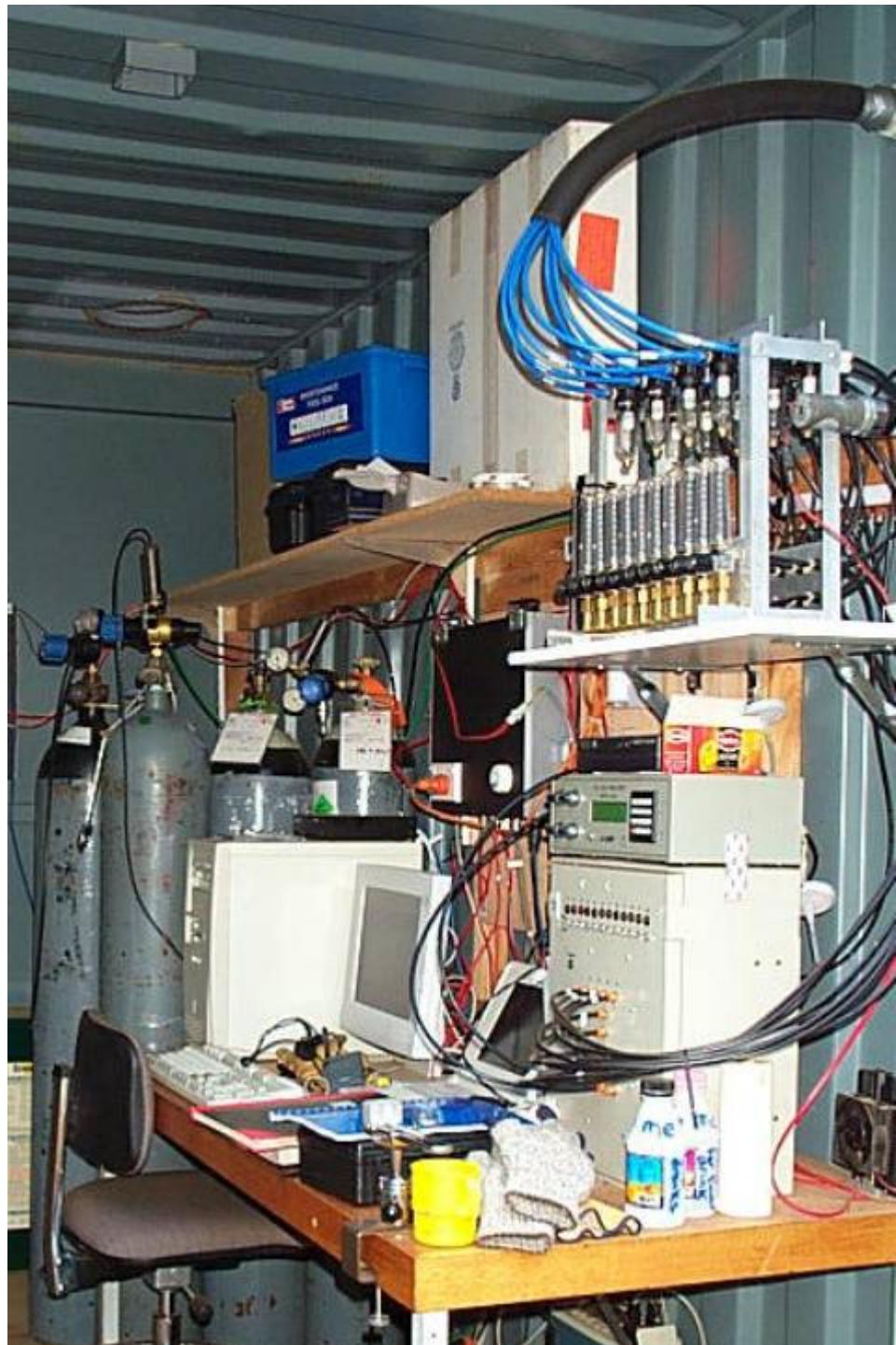
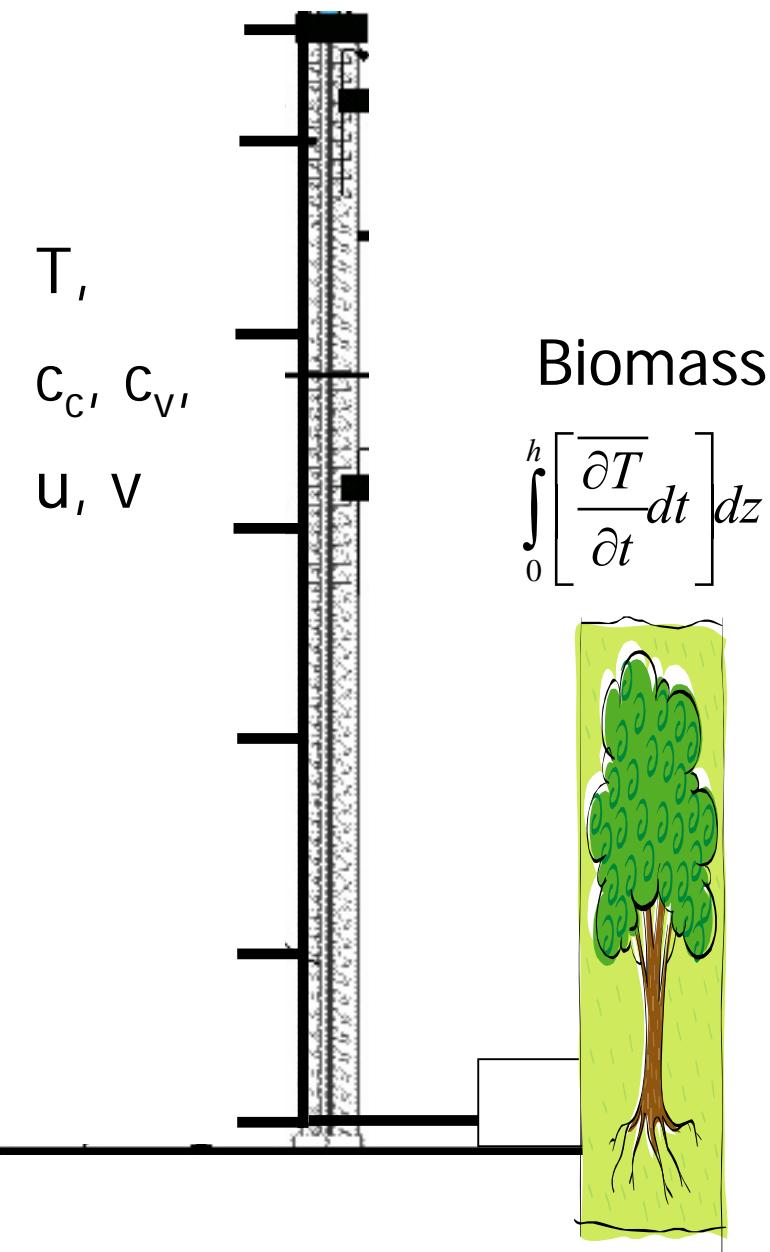
$$= \bar{w}(h) \left[ \bar{\chi}_c(h) - \frac{\int_0^h \bar{\chi}_c(z) u(z) dz}{\int_0^h u(z) dz} \right]$$

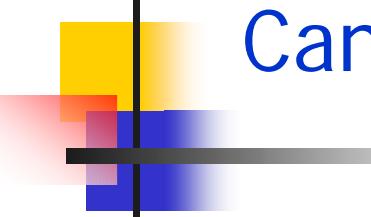
Vertical velocity  
at top of CV

Mixing ratio  
at top of CV

Windspeed-weighted  
mixing ratio within CV

# Profiles





# Canopy Energy Closure at Tumbarumba

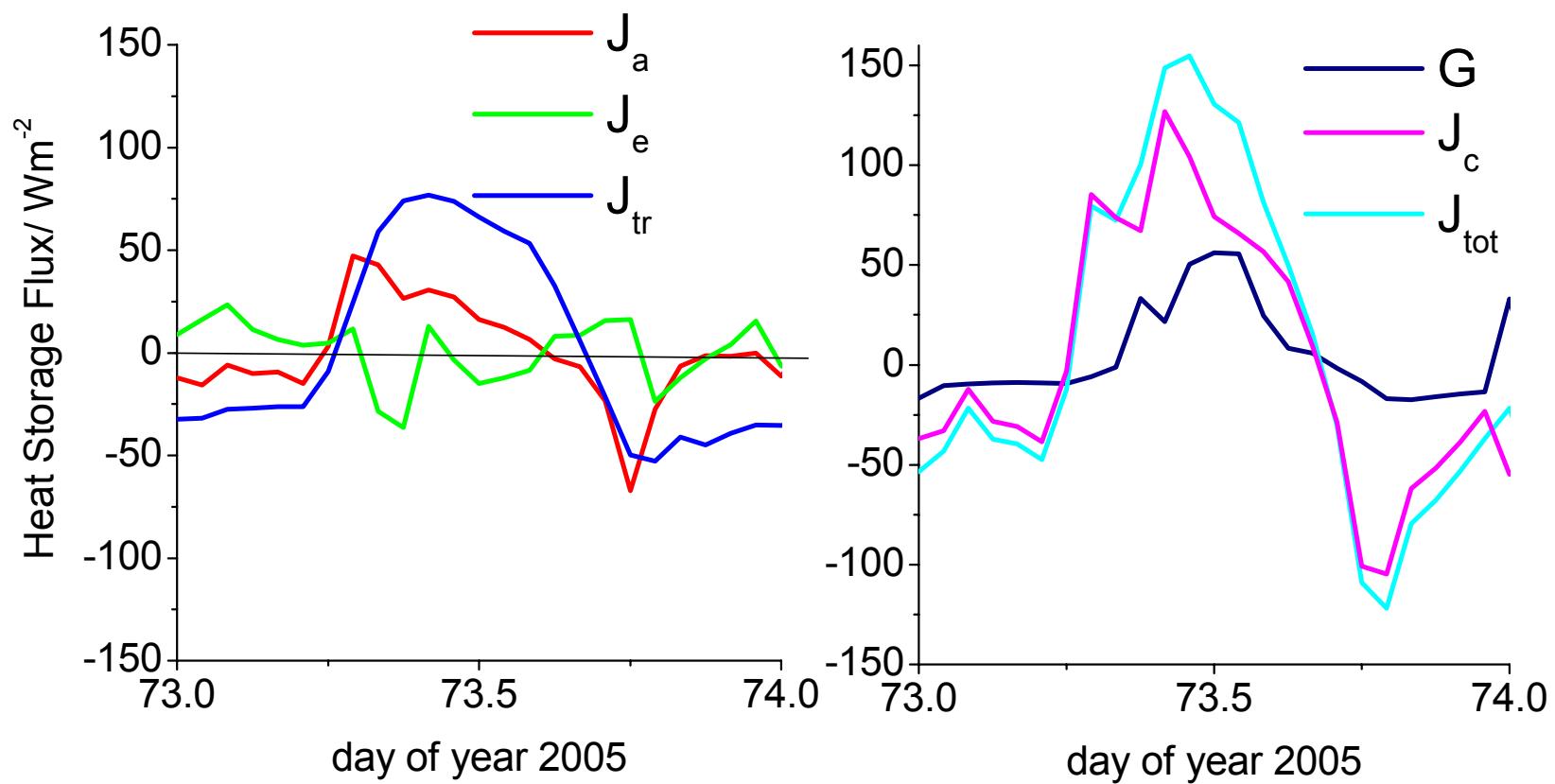
$$R_n - G_0(-\Delta J_c) = H + \lambda E$$

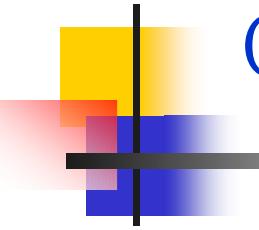
$$J_c = J_a + J_e + J_{tr}$$

Air	H <sub>2</sub> O vapor	Trunks
-----	------------------------	--------

$$J_{tr} = \int_0^{h_c} m_{tr} c_{tr} \frac{d\overline{T}_{tr}(z)}{dt} dz$$

# Magnitude of biomass heat storage term





# Canopy Energy Balance

$$R_n - G_0(-\Delta J_c) = H + \lambda E$$

